

Arc Hazard Analysis Report For Lake Worth T&D System

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City of Lake Worth

Arc Hazard Analysis Report

I. ARC FLASH ASSESSMENT - SCOPE

UC Synergetic, Inc. (UCS) performed an arc flash analysis of the City of Lake Worth (Lake Worth) transmission and distribution system. This report summarizes the assumptions, procedure, and results of the analysis.

Based on the documentation provided by Lake Worth, including the delivery point impedance from Florida Power & Light (FPL), a fault current and arc flash analysis was performed on the Lake Worth T&D system. Milsoft© and ARCPRO™ software tools were used to model and document results for the system. Since upstream protective devices at the FPL delivery point are unknown, arc flash calculations begin at Lake Worth's transmission bus. From there, each of Lake Worth's substations and respective feeders were modeled to complete the power system.

II. ANALYSIS PARAMETERS

Per IEEE 1584a, for voltages over 15 kV the "Lee Method" is recommended to compute the arc flash incident energy and working distances. Industry experience has shown that this methodology is excessively conservative. UCS performed the Lee Method analysis on the Lake Worth transmission and higher voltage distribution system and found multiple locations where incident energy values were such that energized work could not be performed, or the level of PPE required was impractical for the work tasks performed and the local climate. This is consistent with the findings of other utilities. For that reason, utilities operating systems above 15 kV have utilized Table 410-2 "Clothing and clothing systems – voltage, fault current, and maximum clearing time for voltages 46.1 to 800 kV" from the 2007 edition of the National Electric Safety Code (NESC), subsequently updated via Tentative Interim Amendment Table 410-2 "...for voltages 46.1 to 800 kV" issued in September 2008 by the

NESC. These tables show the clothing system required given ranges of bolted fault current and the maximum clearing time for various voltage levels.

UCS calculated specific incident energy values using ARCPRO™. ARCPRO™ is a specially designed arc flash calculator developed by Ontario Hydro Technologies (now Kinetrics), whose calculations were used to produce the NESC tables stated above. A limitation of ARCPRO™ methodology is that the results calculated are limited to open air single phase-to-ground arcs. They are not intended for phase-to-phase arcs or enclosed arcs ("arc in a box"). However, ARCPRO™ results can be adjusted for these conditions using the following adjustment factors for three-phase arcs and "arc in a box" conditions using the following factors recommended by ARCPRO™ documentation.

Scenario	Adjustment Factor – Multiply by
1-phase arc in a box	1.5
3-phase open air arc	1.2 to 2.2
3-phase arc in a box	3.7 to 6.5

Table 1 - ARCPRO Recommended Multipliers for Various Conditions

For the analysis, the highest adjustment factors were used to account for the worst case scenario. The values shown in the NESC tables are reported in increments of 5000 amps (Table 410-1, voltages to 46kV) and 10000 amps (Table 410-2, voltages 46.1 to 800 kV). Actual fault levels provided by Lake Worth or calculated from the impedance model were used. Since Lake Worth is fed at 138kV transmission voltage and utilizes both 26.4 kV and 4.16 kV distribution voltages, ARCPRO™ provides reasonable incident energy calculations consistent with industry practice. For consistency, ARCPRO methodology was used on the 4.16 kV distribution system also.

Milsoft© was used to model the distribution system. The models were built based on drawings provided by Lake Worth. Since a detailed system model was not available, UCS modeled the system with sufficient accuracy to capture the ranges of fault current experienced on each feeder and to confirm values provided by Lake Worth. Each substation was modeled with a source, the relay, and then the backbone of the feeder. The longest fused tap on each feeder was also modeled (if applicable) to show incident energy values beyond a fuse as the protective device and to capture the lower ranges of fault current on each feeder. Based on information provided by Lake Worth, there are no reclosers on any of the distribution feeders.

The source for each of the feeders represents the corresponding 4.16kV or 26.4kV bus. To model the source impedance at each bus, the fault current values, provided by Lake Worth were entered into Milsoft© and then calculated. Relay settings were then used to determine the fault clearing times for the representative fault current levels.

A. Assumptions

Given the lack of specific data in some instances, the following assumptions were used in the analysis.

- 1. The City of Lake Worth's transmission system is fed by Hypoluxo and Canal Substations which are owned and operated by FPL. Lake Worth also operates generation at the Main Plant substation. The source impedances at these substations were provided.
- 2. At Lake Worth substations, any parallel transformers are assumed to be operated with the bus tie switch open; none are operating in parallel. If the bus tie switched is closed and the transformers are paralleled, the fault currents could be as much as two times the levels reported.
- 3. Since detailed power flow and relay data for the transmission system was not provided, all transmission relays are assumed to have instantaneous settings enabled and can reach to the end of their protective range(s). Results for the 138 kV system are shown for fault clearing times of 3, 6, and 12 cycle clearing times at IEEE 516 Minimum Approach Distance. UCS considers 6 cycles to be a conservative estimate for clearing time for higher voltage facility protective devices. Prior to performing any energized work on the transmission system, proper clearances shall be obtained to ensure instantaneous trip is enabled at both ends and automatic reclosing is disabled. A regular testing and maintenance program should be utilized to ensure proper operation of relays and breakers.
- 4. Typical X/R ratios for each transformer were assumed based on the MVA rating of the transformer.
- 5. Ratings and some locations for individual lateral fuses were not known. Where a fuse was identified on a drawing, a 65 amp type T fuse was assumed with the following exceptions.
 - 7th Ave. 4kV Station 704 feeder, Davis Road 4kV Station DR01 feeder, Main 26kV Station 26B1E03 feeder, & East Switching Station 26kV 26B5002 feeder, for which no fuse zones could be identified on the map,

Canal 26kV Station - Feeders 26B6003 and 26B6004, & Main 26kV Station - 26BW13
 feeder, where 80 T fuses were modeled due to the feeder lengths.

Where smaller fuses are used, the arc will be extinguished faster and thus lower incident energy level will result. If larger fuses are known to exist, the energy levels will be higher and should be verified. If a lateral is not fused, or the fuse is too large to coordinate with the upstream device, the relay settings will determine the clearing time and may result in longer arc duration and a higher incident energy level.

6. It is assumed that for all energized work, the overcurrent relay's instantaneous trip is enabled and automatic reclosing is disabled.

III. TRANSMISSION AND DISTRIBUTION SYSTEM ANALYSIS

A. Transmission System Analysis

Incident energy levels for the 138 kV system were calculated using the fault current levels provided at each location. In addition, the incident energy was calculated at two working distances: 3.1 feet (representing line to ground work) and 4.51 feet (representing line-to-line work) based on IEEE 516 Minimum Approach Distances; and at three assumed fault clearing times: 3, 6, and 12 cycles. Results are shown for both single phase open air arcs, computed directly by ARCPRO™, single phase arc in a box using the 1.5 multiplier from Table 1, and phase-to-phase open air arc using the 2.2 multiplier from Table 1. Given the phase separation at 138 kV, three phase enclosed arcs are unlikely, but the values could be calculated using the 6.5 multiplier from Table 1.

The 138 kV results table can be found in Appendix A: Transmission System Results.

B. Distribution System Analysis

Using the Milsoft© models of each substation and feeder, selected points on each feeder were chosen to perform the arc flash analysis. Basic points chosen along each feeder are: just beyond the breaker (JBB), end of breaker zone (EOBZ), just beyond the fuse, and end of fuse zone (EOFZ). Long fused taps were modeled and incident energy was calculated to determine arc flash analysis at low levels of fault current. The results show that fused taps have lower incident energy for two reasons: (1) lower fault currents mean lower energy intensity and (2) fuses have fast clearing time.

For all arc flash analysis, it is assumed that during work on energized devices, the relay instantaneous is enabled, and automatic reclosing is "off." During the course of the study, Lake Worth personnel checked the instantaneous settings on relays and confirmed that in all cases they are set to reach the end of their respective zones. Initial data provided indicated that in some cases instantaneous settings were either disabled or set too high to reach through the breaker's protective zone. If instantaneous trip is not utilized under normal conditions, alternate settings can be used on electronic relays to ensure instantaneous trip is enabled during energized line work.

Two tables show the arc flash analysis calculations: one for the 26.4 kV system and one for the 4.16 kV system. Incident energy was calculated at three distances – 18, 48, and 72 inches. The eighteen-inch results reflect typical industry accepted working distance for gloving applications. The four-foot (48") results represent working distances associated with the use of a five-foot hot stick; while the six-foot (72") results represent working distances associated with an eight-foot hot stick. For each working distance, the incident energy is shown for four scenarios: (1) a single phase open air arc calculated directly by ARCPRO, plus additional scenarios calculated using the highest values in Table 1 above: (2) a single phase arc "in a box" scenario using a 1.5 multiplier, (3) a three phase open air arc using a 2.2 multiplier, and (4) a three phase arc in a box scenario using a 6.5 multiplier. The arc flash boundary (the point at which the incident energy level decreases to a "just curable burn" value of 1.2 cal/cm²) is provided for each scenario as well.

Both tables can be found in Appendix B: Distribution System Results.

IV. FINAL CONSIDERATIONS

When calculating incident energy levels, it is assumed that the devices are operating as designed and that the instantaneous or fast trip is enabled. It is imperative when performing energized line work to ensure that the instantaneous trips are enabled and automatic reclosing is disabled. Furthermore, a regular maintenance program is essential to ensure devices are operating as designed. Incident energy levels during arc flash events are dependent on the fault clearing time and could be significantly higher if a fast trip curve is disabled, non-operational, or altered for any reason.

The results are based on data provided by the City of Lake Worth at the time of the assessment. Since some settings were unavailable, certain engineering assumptions and reasonable conditions were

used to produce a complete model. The energy levels and arc flash boundaries were calculated by the fault current levels and device clearing times computed from the following software programs ARCPRO™ and Milsoft©.

This study should be considered a guide in determining appropriate engineering controls, work practices, and personal protective equipment (PPE) to be utilized by qualified personnel performing energized line work. It is offered as a starting point, not a substitute for, a comprehensive and ongoing safety and training program in the practices and procedures associated with working on energized electrical facilities. Furthermore, it is absolutely essential that following any alterations to the system such as changes by FPL to their facilities, an adjustment to the relay settings or protection scheme, or reconductoring or re-switching of the generation, transmission, or distribution system; that a re-evaluation of the assessment be undertaken.

V. REFERENCES

The following references, standards, and guides were used for this analysis. The standards referenced are current at the time of this analysis. As standards evolve, energy levels and working distances should be re-evaluated.

IEEE Std 1584-2002: "IEEE Guide for Performing Arc Flash Hazard Calculations"; IEEE Industry Applications Society; amended as IEEE Std 1584a-2004 – Amendment 1, 23 September 2004.

National Electric Safety Code (NESC), ANSI C2-2007; Part 4: "Rules for the Operation of Electric Lines"; IEEE

Tentative Interim Amendment 2007-5 to the NESC, 5 September 2008; Revision to Table 410-2: "Liveline tool work clothing and clothing systems – voltage, fault current, and maximum clearing time for voltages 46.1 to 800 kV".

IEEE Std 516-2009 "IEEE Guide for Maintenance Methods on Energized Power Lines", 24 June 2009; IEEE Power and Energy Society.

NFPA 70E-2009 "Standard for Electrical Safety in the Workplace"; National Fire Protection Association

Appendix A

Transmission System Results

	Lake Worth 138 kV Arc Flash Results														
			Fault Durat	Energy (ca tion (cycles e Open Air	s) Single	Fault D	Energy (ca Juration (cy Phase Arc i	cles)	Incident Energy (cal/cm²) at Fault Duration (cycles) Phase to Phase Open Air Arc						
	Fault Current														
Location	(Ph-G)	Distance ⁽¹⁾	3	6	12	3	6	12	3	6	12				
	23099	3.10 ft.	0.767	1.530	3.070	1.151	2.295	4.605	1.687	3.366	6.754				
FPL Cedar	23099	4.51 ft.	0.363	0.727	1.450	0.545	1.091	2.175	0.799	1.599	3.190				
	AF Bo	undary (in.):	30	42	60	38	53	75	55	77	110				
	12928	3.10 ft.	0.363	0.726	1.45	0.545	1.089	2.175	0.799	1.597	3.190				
Hypoluxo		4.51 ft.	0.172	0.344	0.688	0.258	0.516	1.032	0.378	0.757	1.514				
	AF Bo	undary (in.):	21	29	41	26	36	51	39	53	75				
	9588	3.10 ft.	0.251	0.502	1.000	0.377	0.753	1.500	0.552	1.104	2.200				
Main		4.51 ft.	0.119	0.238	0.475	0.179	0.357	0.713	0.262	0.524	1.045				
	AF Bo	undary (in.):	18	24	34	23	30	43	33	44	62				

Notes:

⁽¹⁾ IEEE 516 Table D.3 Feet, For Work Between 72.6 and 121 kV: Minimum Approach Distances

Line to Ground Work: MAD = 3.10 ftLine to Line Work: MAD = 4.51 ftAssume T = 3.0 per NESC Rule 441.A4a

⁽²⁾ Assumed Arc Gap = 7.968 inches per NESC Table 410-2 Note 1

 $^{^{(3)}}$ Multiplier for Single Phase Arc in a Box = 1.5 per ArcPRO Recommendation

⁽⁴⁾ Recommended scenario 6 cycle clearing time but should be verified in field

Appendix B

Distribution System Results

26.4 kV Distribu	ıtion Sy:	stem		Fault Data Zones																		Α	RCPRC	Results	Using '	Worst C	ase for	Each Fe	eder				
																			Worst	18" Rubber Gloving Applications 4' (for 5' Hot Stick Applications) 6' (for 8' Hot Stick Applications)													
Locati	ons		Just l	Beyond	Station	Breaker	En	d of Statio	on Brea	ker Zone	Just Beyond the Fuse (See Note 2)							Case of All Zones		Fault Value x 1.5	Fault Value x 2.2	Fault Value x 6.5		Fault Value x 1.5	Fault Value x 2.2	Fault Value x 6.5		Fault Value x 1.5	Fault Value x 2.2	Fault Value x 6.5		h Boundary al/Cm2)	
Station Name		FDR		Single Phase Fault		@ 18 in	Thre		Duratio	Incident Energy on @ 18 in. s) (cal/cm²)	Three Phase		Duration	@ 18 in.	Three Phas	Single Phase Fault	Duratio n	@ 18 in.		1-Ph Fault Open Air Arc	1-Ph Fault Ard in a Box		3-Ph Fault Arc in a Box		1-Ph Fault Arc in a Box		3-Ph Fault Arc in a Box	-	1-Ph Fault Arc in a Box		3-Ph Fault Arc in a Box		3-Ph (inches)
Main 26 kV Station		BE09	7357	8760	(-)	1.3	34 51	19 478	7 55	5.3 7.09	5119	4787	1.8	0.2	3 500	4624	4 1.9	0.233	EOBZ	7.0	10.64	4 15.60	46.09	1.0	1.52	2.22	6.57	0.45		0.99	2.92	44.5	81.58
Main 26 kV Station	26E	B1E03	7357	8760	9	2.4	2 63	671	8	9 1.74	,		,		*	*	* ,		JBB	2.4	2 3.63	5.32	15.73	0.34	0.52	0.76	2.24	0.15	5 0.23	0.34	0.99	26	47.67
Main 26 kV Station	26E	B1E12	7357	8760	28	7.5	2 44	<mark>64</mark> 389	9	63 6.27	4464	3899	2.8	0.27	9 488	4442	2 3.2	0.372	JBB	7.5	2 11.28	3 16.54	48.88	1.0	1.61	2.35	6.96	0.48	3 0.71	1.05	3.09	45	82.50
Main 26 kV Station	261	BW05	6884	8194	32	7.9	34	277	1 1	09 7.23	4058	3524	2.8	0.24	38	3280	3.2	0.258	JBB	7.9	2 11.88	17.42	51.48	1.13	1.70	2.49	7.35	0.50	0.75	1.10	3.26	46	84.33
Main 26 kV Station	261	BW13	6884	8194	32	7.9	38	333	3	81 6.75	4155	3656	3.9	0.3	389	333	3 4.8	0.396	JBB	7.9	11.88	17.42	51.48	1.13	1.70	2.49	7.35	0.50	0.75	1.10	3.26	45	82.50
7th Ave. North Statio	on 268	B0701	5129	4761	18	2.2	2 <mark>9</mark> 43	377	3	23 2.20	4366	3773	2.5	0.23	9 418	3562	2.8	0.25	JBB	2.2	9 3.44	5.04	14.89	0.33	0.49	0.72	2.12	0.15	0.22	0.32	0.94	25	45.83
Canal 26 kV Station	268	B6003	3733	3042	32	2.3	26	194	4	68 2.83	2676	2007	10.3	0.44	7 259	1920	11.2	0.458	EOBZ	2.8	4.25	6.23	18.40	0.40	0.60	0.88	2.61	0.18	3 0.27	0.39	1.16	28	51.33
Canal 26 kV Station	268	B6004	3733	3042	32	2.3	28	214	2	57 2.70	2830	2142	9.1	0.41	5 272	2042	2 10	0.426	EOBZ	2.7	0 4.05	5.94	17.55	0.38	0.58	0.84	2.50	0.17	7 0.26	0.38	1.11	27	49.50
East Switching Station		B5002	6366	6735	5	0.9	54	517	4	32 4.51			,		*	×	·		EOBZ	4.5	6.7	9.92	29.32	0.64	0.96	1.41	4.17	0.29	0.43	0.63	1.85	35	64.17
East Switching Station	on 261	B5003	6366	6735		0.9	48	443	2	36 4.21	4854	4432	2	0.2	3 475	4302	2.1	0.234	EOBZ	4.2	6.32	9.20	27.37	0.60	0.90	1.32	3.90	0.27	0.40	0.59	1.74	34.5	63.25
18th Ave.	268	B1801	4310	3804	23	2.2	25 35	296	1	31 2.23	3592	296	3.8	0.27	348	284	3	0.27	JBB	2.2	3.38	4.9	14.63	0.32	0.48	0.70	2.08	0.14	0.21	0.31	0.92	25	45.83

- 1. Circuits where no fuse zone could be identified on the map are marked with an *.
- 2. All circuits were modeled using 65 T Fuse for the Fuse Zone with the exception of 26B6003, 26B6004, and 26BW13 where 80 T fuses were modeled due to the feeder length
- 3. Circuit 26B5003 was assumed to have the same relay settings as 26B5002 as well as 26B1E12 having the same relay settings as 26B1E03.
- 4. JBB = Just Beyond Station Breaker; EOBZ = End of Station Breaker Zone; EOFZ = End of Fuse Zone
- 5. Arc Gap = 6 inches per NESC

															Usin	g Alternat	e Settings	with Instanta	neous Set	(See Notes	Below)											
26 4 kW Dietribusie		Fault Data Zones																			^	PCPPC	Poculto	Heina	Worst C	aso for	Each E	oodor				
26.4 kV Distributio	n System																	Worst	18" Rı	ARCPRO Results Using Worst Case for Each Feeder 18" Rubber Gloving Applications 4' (for 5' Hot Stick Applications) 6' (for 8' Hot Stick Applications)										cations)		
																Case of	10 110	I-PII T-PII I-PII				I-PN	1-Ph	1-P11	0 (.0.	I-PN						
		Just	Beyond	Station	Breaker	Fn	nd of Statio	n Break	er Zone	Jus	t Bevond	the Fue	se (See	End of Fuse Zone (See			All Zones		Fault Value x	Fault Value x	Fault Value x		Fault Value x	Fault Value x	Fault Value x		Fault Value x	Fault Value x	Fault Value v	Arc Flasi	n Boundary	
Locations	5		stantane				Instantane			Just Beyond the Fuse (See Note 2)						ote 2)	(500)	(4)		1.5	2.2	6.5		1.5	2.2	6.5		1.5	2.2	6.5		al/Cm2)
		ì			Inciden				Incident				Incident			Fault	Incident		1-Ph		3-Ph		1-Ph		3-Ph		1-Ph		3-Ph			,
		Three	Single	Fault	Energy		Single	Fault	Energy		Single	Fault	Energy	Three	Single	Fault Duratio			1-Ph Fault	1-Ph	3-Pn Fault	3-Ph	1-Pn Fault	1-Ph	3-Pn Fault	3-Ph	1-Pn Fault	1-Ph	3-Pn Fault	3-Ph		
		Phase	Phase	Duration		Phas	se Phase	Duration	n @ 18 in.	Phase	Phase	Duration	@ 18 in.	Phase	Phase	n	@ 18 in.		Open Ai	Fault Arc	Open Air	Fault Arc				Fault Arc	Open Air			Fault Arc	Ph-G	3-Ph
Station Name	FDR	Fault	Fault	(Cycles)	(cal/cm	²) Faul	lt Fault	(Cycles) (cal/cm²)	Fault	Fault	(Cycles)	(cal/cm ²)	Fault	Fault	(Cycles)	(cal/cm ²)		Arc	in a Box	Arc	in a Box	Arc	in a Box	Arc	in a Box		in a Box	Arc	in a Box	(inches)	(inches)
Main 26 kV Station	26BE09	7357	8760	5	5 1.3	51	4787	7	5 0.64	5119	4787	1.8	0.23	500	462	4 1.9	0.233	JBB	1.3	4 2.0 ²	2.9	8.71	0.19	0.29			0.09		0.19	0.55	19	34.83
Main 26 kV Station	26B1E03	7357	8760	5	1.3	63 63	3 53 6718	3	5 0.97	7	*		,	100	*	* *		* JBB	1.3	4 2.0	2.9	8.71	0.19	0.29			0.09		0.19	0.55	19	34.83
Main 26 kV Station	26B1E12	7351	8760		1.3	44	3899	9	5 0.50	4464	3899	2.8	0.279	488	4442	2 3.2	0.372	IBB	1.3	4 2.0	2.9	8.71	0.19	0.29		1.24	0.09		0.19	0.55	19	34.83
Main 26 kV Station	26BW05	600	8194	5	1.2	24 34	200 222	1	5 0.33	4058	3524	2.0	0.248	385	328	3.2	0.258	JBB	1.2	4 1.86		8.00	0.18	0.26		1.14	0.08		0.17	0.51	19	34.83
Main 26 kV Station 7th Ave. North Station	26BW13 26B0701	5120	0194 4761	5	1.2	4 30	355	3	5 0.42	4155	3773	3.8	5 0.30	J08	356	2 2.9	0.390	JDD IRR	0.6	4 1.86	5 2.7	0.00	0.10	0.26		0.50	0.08		0.17	0.51	19	34.83 23.83
Canal 26 kV Station	26B6003	3733	3042	-	5 0.0	37 26	377	4	5 0.40	2676	2001	10.3	3 0.447	250	2 192	2.0 6 11.2	0.25	EOFZ	0.0	6 0.90	3 1.40	2.96	0.03	0.14		0.39	0.03			0.20	11	20.17
Canal 26 kV Station	26B6004	3733	3042	5	0.3	37 28	330 2142	2	5 0.24	0000	2142	9.1	0.447		0 204	2 10	0.426		0.4	3 0.64	4 0.94	4 2.77			0.14	0.41	0.03		0.06	0.13	12	22.00
East Switching Station	26B5002	6366	6735	5	0.9	7 54	111 5174	4	5 0.70		*	,	*		*	* *	0.12	* JBB	0.9	7 1.45	5 2.12	2 6.27	0.14	1 0.21	0.31	0.90	0.06		0.14	0.40	17	31.17
East Switching Station	26B5003	6366	6735	5	0.9	97 48	354 4432	2	5 0.59	4854	4432	2	2 0.23	475	7 430	2 2.1	0.234	JBB	0.9	7 1.45	2.12	2 6.27	0.14	0.21	0.31	0.90	0.06		0.14	0.40	17	31.17
18th Ave.	26B1801	4310	3804	5	0.4	9 35	296	1	5 0.36	3592	2961	3.8	0.272	348	3 284	3 4	0.27	1 JBB	0.4	9 0.73	3 1.0	3.17	0.0	0.10	0.15	0.45	0.03	0.05	0.07	0.20	12	22.00

- 6. Phase Instantaneous of 2400 Amps and Ground Instantaneous of 1200 Amps will cover all conditions with sufficient margin
- 7. Individual instantaneous settings can be used at each feeder, provided:

Phase pickup is set below the three phase fault current at end of station breaker zone.

Ground pickup is set below the single phase fault current at end of station breaker zone.

(Recommend additional safety margin to ensure instantaneous operation, e.g. set to 80% of fault current to be cleared)

4.16 kV	Distribution	System																ARCPRO Results Using Worst Case for Each Feeder 18" Rubber Gloving Applications 4' (for 5' Hot Stick Applications) 6' (for 8' Hot Stick Applications)															
																			Worse Case of	18" Ru	ibber Glov				5' Hot Sti	ick Applic	cations)	6' (for	8' Hot Sti	ck Applic	ations)		
	Locations		luet F	Sevond :	Station	Broakor	Fne	d of Statio	n Break	er Zone	Ji	ust Beyo	nd the F	use	En	End of Fuse Zone (Assume 65T)					1-Ph Fault Value x 1.5	1-Ph Faul Value x 2.2	t 1-Ph Fault Value x 6.5	t	1-Ph Fault Value x 1.5	1-Ph Fault Value x 2.2	1-Ph Fault Value x 6.5		1-Ph Fault Value x 1.5	1-Ph Fault Value x 2.2	1-Ph Fault Value x 6.5		h Boundary
	Locations		Just	Jeyona	Station	Incident		d or Statio	II Break	Incident		(Assur	iie 031)	Incident			31)	Incident	Zones													(1.2 0	aironiz)
			Three Phase	Phase	Fault Duration		Phas	e Phase	Fault Duration		Phase		Fault Duration		Phase		Fault Duration	@ 18 in.		Open Air	t 1-Ph Fault Arc in a	Open Air	Arc in a	Open Air	Arc in a	Open Air	Arc in a	Open Air	Arc in a	Open Air	Arc in a	Ph-G	3-Ph
	ion Name	FDR	Fault	Fault	(Cycles)	(cal/cm²)	Faul	t Fault	(Cycles)	(cal/cm ²)	Fault	Fault	(Cycles)	,	Fault	Fault	(Cycles)	(cal/cm ²)		Arc	Box	Arc	Box	Arc	Box	Arc	Box	Arc	Box	Arc	Box	(inches)	(inches)
4th Ave.		401	8153	8820	5	0.65	190	1442		5 0.05 5 0.07	1936	1442	10.5	0.118	187	1390	11	0.117	JBB	0.68	0.97	1.42	4.19	0.09	0.13	0.19	0.56	0.04		0.08	0.25	18	33.00
4th Ave.		402 404	8153	8820	5	0.65		90 1654	· ·	5 0.07	2190	1654	3.4	0.107	214	8 1617 4 2254	8.4	0.111	JBB	0.68	5 0.97 5 0.97	1.42			0.13			0.04 0.04		0.08	0.25	18.5	33.92 23.83
4th Ave.		601	8012	8820 8684	5	0.65		42 3670 73 2434		5 0.20 5 0.12	3073	3670 2434	2.4	0.10	295	6 2254	4.5	0.10	JBB	0.63	0.97	1.42	4.19 4.11	0.09	0.13 0.13	0.19	0.56 0.55	0.04	0.06	0.08	0.25 0.24	13	29.33
6th Ave.		602	8012	8684	5	0.63		56 1627	ì	5 0.12	2156	1627	9	0.03	154	6 1132	16	0.10	JBB	0.00	3 0.95	4.00	9 4.11	0.00	0.13	0.19	0.55	0.04	0.06	0.00	0.24	18	33.00
6th Ave.		604	8012	8684	5	0.63		60 3397	ì	5 0.18	4060	3397	26	0.09	308	2444	4.2	0.13	JBB	0.63	3 0.95	1.39	9 4.11	0.08	0.13	0.13	0.55	0.04	0.00	0.00	0.24	13	23.83
7th Ave.		701	7872	8556	5	0.62		93 1748		5 0.07	2293	1748	7.4	0.10	188	1403	10.5		JBB	0.62	2 0.93	1.36			0.12	0.18	0.54	0.04	0.05	0.08	0.24	17.5	32.08
7th Ave.		702	7872	8556	5	0.62		74 1316		5 0.05	1774	1316	19	0.19	170	1257	20	0.19	JBB	0.62	2 0.93	1.36	4.03	0.08	0.12	0.18	0.54	0.04		0.08	0.24	13	23.83
7th Ave.		704	7872	8556	5	0.62		16 1031		5 0.03	*	*	*	,		* *	*	*	JBB	0.62	2 0.93	1.36	4.03	0.08	0.12	0.18		0.04		0.08	0.24	22	40.33
11th Ave.		1101	13388	15724	5	1.48		71 2143		5 0.10	2871	2143	5	1.01	256	1895	7	0.11	JBB	1.48	2.22			0.19	0.29	0.43	1.26	0.09	0.13	0.19	0.56	20	36.67
11th Ave.		1102	13388	15724	5	1.48	398	80 3089		0.16	3980	3089	3	0.09	322	2436	4	0.09	JBB	1.48	8 2.22	3.26	9.62	0.19	0.29	0.43	1.26	0.09	0.13	0.19	0.56	20	36.67
11th Ave.		1103	13388	15724	5	1.48	206	<mark>65</mark> 1500		0.06	2065	1500	10	0.12	179	1293	13	0.13	JBB	1.48	2.22	3.26	9.62	0.19	0.29	0.43	1.26	0.09	0.13	0.19	0.56	20	36.67
11th Ave.		1104	13388	15724	5	1.48	24	73 1821		0.08	2473	1821	7	0.11	231	2 1693	8	0.11	JBB	1.48	8 2.22	3.26	9.62	0.19	0.29	0.43	1.26	0.09	0.13	0.19	0.56	20	36.67
12th Ave.		1201	8487	9206	5	0.69	298	89 2337		5 0.11	2989	2337	5	0.11	227	'9 1720	8	0.11	JBB	0.69	9 1.03	1.51	1 4.46	0.09	0.14	0.20	0.59	0.04	0.06	0.09	0.26	16.5	30.25
12th Ave.		1202	8487	9206	5	0.69	498	57 4304		5 0.25	4957	4304	2	0.10	349	2807	3.4	0.10	JBB	0.69	9 1.03	1.51	4.46	0.09	0.14	0.20	0.59	0.04	0.06	0.09	0.26	13.5	24.75
12th Ave.		1203	8487	9206	5	0.69	138	85 1002		5 0.03	1385	1002	20	0.13	135	982	21	0.13	JBB	0.69	9 1.03	1.51			0.14	0.20	0.59	0.04	0.06	0.09	0.26	22	40.33
12th Ave.		1204	8487	9206	5	0.69	333	35 2654		5 0.13	3335	2654	3.6	0.09	184	1361	12	0.12	JBB	0.69	9 1.03	1.51	4.46	0.09	0.14	0.20	0.59	0.04	0.06	0.09	0.26	16	29.33
15th Ave.		1501	7623	8373	5	0.60	336	2747		0.14	3366	2747	3.5	0.09	286	22 7 0	5	0.10	JBB	0.60	0.90	1.32	3.91	0.08	0.12	0.18	0.52	0.04		0.08	0.23	16.5	30.25
15th Ave.		1502	7623	8373	5	0.60	430	3724		0.20	4305	3724	2.2	0.09	328	2667	4	0.11	JBB	0.60	0.90	1.32	3.91	0.08	0.12	0.18	0.52	0.04		0.08	0.23	13	23.83
15th Ave.		1503	7623	8373	5	0.60	444	46 3881		0.22	4446	3881	2	0.08	319	2581	4	0.10	JBB	0.60	0.90	1.32	3.91	0.08	0.12	0.18	0.52	0.04		0.08	0.23	13	23.83
15th Ave.		1504	7623	8373	5	0.60		2312	,	0.11	2910	2312	5	0.11	267	5 2097	5.3	0.10	JBB	0.60	0.90	1.32		30.0	0.12	0.18		0.04	0.05	0.08	0.23	17.5	32.08 31.17
18th Ave.		1802 1803	7829	8666	5	0.63		78 1323		5 0.10 5 0.05	2800 1770	1323	5	0.10	230	1813	15	0.11	JBB	0.63	0.94	1.38	3 4.06 3 4.06	0.08	0.13	0.18	0.54	0.04 0.04	0.06	0.08	0.24	17	31.17
18th Ave.		1804	7829	8666 8666	5	0.63		78 1323 79 2006		5 0.05 5 0.09	2570	1323	12	0.12	250	1 196	6.2	0.13	JDD	0.63	3 0.94	1.30	4.06	0.00	0.13	0.40	0.54	0.04	0.06	0.00	0.24	17	31.17
Davis Roa	d	DR01	8377	9005	5	0.63		79 2006 04 1251		5 0.09	2519	2006	*	0.10	232	* * *	V.Z	0.10	JBB	0.63	0.94	1.30	4.00	0.08	0.13	0.18	0.54 0.57	0.04	0.06	0.08	0.24	21	38.50
Main 4kV		3S03	11627	12758	5	1.10		67 2569		5 0.03	3367	2569	1	0.10	279	2083	5.5	0.10	JRR	1 10	1.00	2.42		0.08	0.13	0.18	0.57	0.04	0.10	0.08	0.23	17.5	32.08
Main 4kV		3S04	11627	12758	5	1.10	229	84 1676		5 0.12	2284	1676	8	0.10	228	1676	10	0.10	JRR	1.10	0 1.65	2.42		0.14	0.22	0.32	0.94	0.06	0.10	0.14	0.42	17.5	32.08
Main 4kV		3S05	11627	12758	5	1.10	238	89 1767		5 0.07	2389	1767	72	0.11	227	0 1665	8	0.14	JBB	1.10	0 1.65				0.22	0.32		0.06	0.10	0.14	0.42	17.5	32.08
Main 4kV		3N11	11562	14039	5	1.25	31	16 2357		5 0.11	3116	2357	4	0.09	261	7 1944	6	0.10	JBB	1.29	1.88	2.75		0.17	0.25	0.36	1.07	0.07	0.11	0.16	0.48	18.5	33.92
Main 4kV		3N12	11562	14039	5	1.25		29 1554		5 0.06	2129	1554	9	0.11	205	1493	10	0.12	JBB	1.25	5 1.88	2.75		0.17	0.25	0.36	1.07	0.07	0.11	0.16	0.48	18.5	33.92
Main 4kV		3N13	11562	14039	5	1.25		43 1724		5 0.07	2343	1724	8	0.11	217	5 1591	9	0.12	JBB	1.25	1.88		8.13	0.17	0.25	0.36	1.07	0.07	0.11	0.16	0.48	18.5	33.92

- Notes: 1. Circuits where no fuse could be identified on the map are marked with an st.
- 2. All circuits were modeled using 65 T Fuse for the Zone Fuse.
- 3. JBB Just Beyond Breaker, EBZ End of Station Breaker Zone, JBF Just beyond the Fuse; EFZ End of the Fuse Zone